

DOMANEVSKIY, Nikolay Alekseyevich; GOLOVUSHKIN, N.I., retsenzent;  
SHAROV, I.M., retsenzent; SKOROSHCHINSKIY, V.F., red.;  
FILIMONOVA, A.I., red.

[Dredging] Dnougublennie. Moskva, Transport, 1965. 339 p.  
(MIRA 18,12)

MEZENTSEV, O.K.; RATNIKOV, V.M.; SKOROSPEL'KIN, S.A.

Statistical treatment of the data of geochemical prospecting.  
Razved. i okh. nedr 30 no.10:10-15 O '64. (MIRA 18:11)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut mineral'nogo  
syr'ya, Moskva (for Mezentsev, Ratnikov). 2. Gosudarstvennyy  
geologicheskii komitet SSSR (for Skorospelkin).

SKOROSPELOV, D.

USSR/ Electronics - Radio combination

Card 1/1            Pub. 89 - 28/30

Authors            :    Ganzburg, M., and Skorospelov, D.

Title              :    Homemade combined radio and phonograph sets

Periodical        :    Radio 3, 59 - 61, Mar 1955

Abstract          :    The schematic drawing is given of the circuit of a homemade combined radio and phonograph set. Directions are also given for constructing the set, most of the parts of which are factory-made but many of which are also made at home. The method of tuning is also explained. Illustrations; drawing; table.

Institution :        .....

Submitted    :        .....

SKOROSPELOV, D.

107-5-19/54

AUTHOR: Ganzburg, M. and Skorospelov, D.

TITLE: A Simple Superheterodyne (Prostoy superheterodin)

PERIODICAL: Radio, 1956, Nr5, pp. 17-19 (USSR)

ABSTRACT: A selfmade superhet radio receiver is described. It has two bands: 150 to 415 kc and 520 to 1.600 kc. Sensitivity at any point is better than 150  $\mu$ v, selectivity 20 db or higher. Nonlinear distortion factor is under 10% at 0.5 w output. A-f pass band of the overall receiver is 100 to 4,000 c with 5 db irregularity. Sensitivity at the pickup jacks 200 mv, background level 26 db. Power consumption 20 w. Bantam tubes. Pentode grounded-plate oscillator. Semiconductor-type two-diode rectifier.

Description of all parts and how to make them with very limited facilities is given; also the schematic, parts, and assembly views. Tube types used: 6A2П, 6K4П, 6Ж3П, 6П1П.

There are 6 figures and one table in the article.

AVAILABLE: Library of Congress.

Card 1/1

BUKHARTSEV, V.P.; SKOROSPELOVA, T.P.; STROYEVA, Ye.A.; USTINOVA, Z.S.

Morphology of lithofacies replacement in the middle Devonian of  
the eastern part of the Russian Platform. Dokl. AN SSSR  
139 no.5:1177-1180 Ag. '61. (MIRA 14:8)

1. Institut geologii i razrabotki goryuchikh iskopayemykh  
AN SSSR. Predstavleno akademikom A.A. Trofimukom.  
(Russian Platform—Geology, Structural)

KULAKOVA, R.Ye., kand.tekhn.nauk; MIRZOYEV, A.G., inzh.; SKOROSPELOVA, Ye.V.  
inzh.

Power cables with polyethylene insulation for 10 kv. voltage. Vest.  
elektroprom. 31 no.3:41-45 Mr '60. (MIRA 13:6)  
(Electric insulators and insulation)  
(Electric cables)

[illegible]

SOV/144-58-12-6/19

AUTHOR: Skorospeshkin, A.I., Aspirant

TITLE: The Reaction of Commutation Currents in Transverse-Field  
Dynamoelectric Amplifiers

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy,  
Elektromekhanika, 1958, Nr 12, pp 47-51 (USSR)

ABSTRACT: In d.c. machines under normal conditions of operation the magnetic effects of commutation currents are only significant under transient conditions. In transverse field rotating amplifiers the commutation currents (c.c.) have a delaying action and also oppose the flux from the control winding. A number of methods have been proposed for calculating reaction effects. That due to Epshteyn is much used but it is laborious and introduces a 'brush overlap coefficient' (Ref 3) which describes commutation incorrectly. M.M. Tarashchanskiy (Ref 4) represents the current in the commutated sector as the sum of rectilinear and auxiliary components. Only the latter cause reaction effects and the estimate is not accurate enough. V.I. Radin (Ref 5) calculates the magnetizing force of the c.c. on the assumption that the resistances of the leading and trailing edges of the brush contact are equal and constant, but the accuracy is no better than with ✓

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1/3



SOV/144-58-12-6/19

The Reaction of Commutation Currents in Transverse-Field  
Dynamoelectric Amplifiers

Epshteyn. The process of commutation is most truly represented by the method due to M.S. Mikhaylov-Mikulinskiy (Ref 8). The commutating circuit is represented by an equivalent network and the auxiliary currents are found by a superposition method. The formulae for these currents in the EMU-5P and EMU-12A amplifiers are respectively Eqs (1) and (2), where  $e_z$  is the resultant e.m.f. of the commutating sector,  $R$  is the transfer resistance when the brush width and collector pitch are equal. The magnetizing force of the c.c. is Eq (3), where  $w_k$  is the number of turns in the commutating sector. Table 1 compares the results of the four methods of calculation with experimental values obtained by M.I. Alyab'yev's method (Ref 7). The agreement is poor. It is therefore proposed to represent the auxiliary current by a sinusoid, as in Fig 1. Since the 'brush overlap coefficient',  $\beta$ , usually lies between 1 and 2 commutation must occur partly in one sector and partly in two. In the latter case the resulting current can be found from the vector diagram of Fig 2, where the

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SOV/144-58-12-6/19

The Reaction of Commutation Currents in Transverse-Field  
Dynamoelectric Amplifiers

shift angle is Eq (6). The demagnetizing force varies between two limits and the average value is Eq (10), or in terms of the branching coefficient  $K$  (Fig 3), Eq (12). Table 2 compares calculations by this formula with experimental results (obtained as before) for three different machines under two conditions of operation. The agreement is very satisfactory. The magnitude of the auxiliary current was calculated from a formula, Eq (11), due to Arnold (Ref 10).

There are 3 figures, 2 tables and 10 Soviet references.

ASSOCIATION: Kafedra elektricheskikh mashin, Tomskiy politekhnicheskoy institut (Chair of Electrical Machines, Tomsk Polytechnical Institute) ✓

Card 3/3

SUBMITTED: December 16, 1958

SOV/144-59-2-8/19  
AUTHOR: Skorospeshkin, A.I., Aspirant  
TITLE: On the Commutation of Small DC Machines  
PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy, Elektromekhanika,  
1959, Nr 2, pp 73 - 75 (USSR)  
ABSTRACT: A study was made of commutation, with particular reference  
to amplidynes, taking the transient brush contact resistance  
to be a function of current. Using the equivalent circuit  
of Figure 1, expression (1) gives the differential equation  
of the current in the commutating section, where  $r_1$  and  
 $r_2$  are the transient resistances of the leading and  
trailing parts of the brush. In formulating the equation  
it is assumed that the brush is the same width as the  
commutator bars and that there is no commutating e.m.f.  
In this equation the two transient resistances are taken  
as functions of current density. An experimental curve of  
transient brush contact resistance as a function of current  
density for a brushgrade EG-8, used in amplidynes, is  
plotted in Figure 2; it is a straight line. The values

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On the Commutation of Small DC Machines SOV/144-59-2-8/19

of  $r_1$  and  $r_2$  required in Eq (1) can be obtained from this curve using Eqs (2), (3) and (4). The current densities are given by Eq (5). Eqs (5) and (4) are then substituted into expression (1) to give the non-linear differential Eq (6). This equation is solved by the method of successive intervals.

Curves calculated in this way are compared with oscillograms for two different experimental cases in Figures 3a and b. In both cases the good agreement between the experimental and the theoretical curves shows that the transient resistance of the brush contact considered as a function of current density has an important influence on the changes in current in the commutating section and so should not be neglected.

There are 3 figures and 6 Soviet references.

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SOV/144-59-2-8/19

On the Commutation of Small DC Machines

ASSOCIATION: Kafedra elektricheskikh mashin, Tomskiy  
politekhnicheskiy institut (Chair of Electrical  
Machinery, Tomsk Polytechnical Institute)

SUBMITTED: May 5, 1958



Card 3/3

AUTHOR: Skorospeshkin. Aleksey Ivanovich, aspirant 59-6-8/15

TITLE: The Commutation of Cross-field Amplidynes

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy, Elektromekhanika,  
1959, Nr 6, pp 66 - 70 (USSR)

ABSTRACT: A study was made of commutation in a cross-field amplidyne, making allowance for the non-linear relationship between the transient resistance of the brush contact and the current density. It is shown that the work of Tur, published in Elektrichestvo, 1956, Nr 11 and relating to a normal DC machine is not applicable. Accordingly the equivalent circuit of Figure 1 was used, which introduces the transient resistance of the brush contact directly. Eq (1) is the differential equation that describes the change of current in the commutating circuit. In formulating this equation it is assumed that there is no commutating e.m.f. and that the brush width is equal to the commutator-bar pitch. An experimental curve of the transient resistance of a brush contact as a function of current density for brushes grade EG-8 used in a cross-field amplidyne is given in Figure 2. This curve may be

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The Commutation of Cross-field Amplidynes

approximately represented by the exponential equation (2). It should be noted that because of manufacturing variations the transient resistance of this grade of brush as a function of current may sometimes be exponential and sometimes linear.

Various subsidiary equations that are required are derived and are substituted in Eq (1) to give Eq (5). The latter was solved for a particular case by the method of successive integration to give Curve 1 of Figure 3. Other curves, corresponding to equations obtained by other authors, are also plotted in Figure 3 to check their validity in relation to a cross-field amplidyne. It will be seen that Curve 1 agrees best with test results. This is because non-linearity of the transient resistance of the brush contact has a considerable influence on the change of the current in the commutating section and should be allowed for in analysis of commutation in cross-field amplidynes. The differences between Curve 1 (theoretical) and Curve 5 (experimental) result partly from the approximate nature of the solution of the differential Eq (5) and partly from

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The Commutation of Cross-field Amplidynes SOV/144-59-6-8/15

disregard of armature reaction in the amplidyne.

The curves of other authors do not in general agree at all well with the experimental values.

There are 3 figures and 5 Soviet references.

ASSOCIATION: Kafedra elektricheskikh mashin, Tomskiy politekhnicheskii institut (Chair of Electrical Machines, Tomsk Polytechnical Institute)

SUBMITTED: March 28, 1959

Card 3/3



SOV/144-59-11-11/21

AUTHOR: Skorospeshkin, A. I. Aspirant

TITLE: Some Results of an Experimental Investigation of the Process of Commutation in a Cross-Field Amplidyne

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy, Elektromekhanika, 1959, Nr 11, pp 74-78 (USSR)

ABSTRACT: The cross-field amplidyne has two sets of brushes, so that the current distribution in the armature winding is not uniform and commutation is poor. There are several stator windings, each of which affects commutation. It was accordingly decided to make tests of commutation in cross-field amplidynes, and this article gives some information on the influence of the compensating winding and interpoles on the process of commutation. If the amplidyne direct-axis armature reaction is not compensated, the amplidyne cannot work, and under- or over-compensation are causes of unstable operation. Sparking is often attributed to the brushes or to out-of-balance when in fact it is due to incorrect compensation. Special tests were made to study the influence of direct-axis armature reaction on the

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SOV/144-59-11-11/21

Some Results of an Experimental Investigation of the Process of  
Commutation in a Cross-Field Amplidyne

commutation of an amplidyne: brushes equal in width to the commutator pitch were fitted on the direct axis; the quadrature-axis brushes were removed and an external supply was applied to the armature winding. A curve of the current in the commutating section is plotted in Fig.2 for an armature current of 1.5 A and shows that commutation conditions are difficult both at the leading and the trailing edges of the brushes. This poor commutation is due to the field of direct-axis armature reaction. The corresponding field curve, shown in Fig.3, indicates that the field reaches a maximum on the axis of the brushes, so that commutation is bad. Thus it is obviously necessary to compensate direct-axis armature reaction. Similar tests were made to study the influence of the compensating winding, but the compensating winding was also supplied from an external source in these tests. The current curve in Fig.4 corresponds to under-compensation of about 47%; conditions are better than in the curve of Fig 2, but

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Some Results of an Experimental Investigation of the Process of  
Commutation in a Cross-Field Amplidyne

still difficult at both leading and trailing edges. The curve of Fig.5 was obtained with normal compensation; here commutation follows the desirable straight-line law. Fig.6 shows a curve corresponding to an over-compensation of 21% and the commutation conditions are again bad. If there are no brushes on the commutator and supply is applied only to the compensating winding, the field curve is as shown in Fig.7. As the armature field is compensated the resultant field curve changes; Fig.8 shows the latter curve when the under-compensation is about 2%. A number of practical conclusions are drawn from this evidence. The influence of the interpoles is then analysed. In normal d.c. machines they are fitted at the neutral position and are the main method of improving commutation. In cross-field amplidynes the main pole is split and the interpole is located in the middle of the main pole so that its operation and effectiveness are somewhat different. Special tests to check the influence of the interpoles on commutation indicated that to obtain straight-line

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307/144-59-11-11/21

Some Results of an Experimental Investigation of the Process of  
Commutation in a Cross-Field Amplidyne

commutation with an armature current of 1.7 A, a current of 6.1 A is necessary in the interpoles. Thus, the effect of the interpoles is not very great and adjustment of commutation depends mainly on the compensating windings. The curve of Fig. 9 was obtained with supply applied only to the interpole winding with no brushes on the commutator. It will be seen that the interpole field curve has a marked peak, but that the interpole is not effective. There are 9 figures and 6 Soviet references.

ASSOCIATION: Tomskiy politekhnicheskii institut  
(Tomsk Polytechnical Institute)

Card 4/4

SKOROSPESHNIK, A. I. Cand Tech Sci -- (diss) "Commutation  
of electrical machine boosters with a lateral field," Tomsk, 1960,  
10 pp, 150 cop. (Tomsk Polytechnical Institute S. M. Kirov) (KL, 42-60, 114)

SERDYUK, Fedor Aleksandrovich, kand.tekhn.nauk; SKOROSPESHKIN,  
Aleksey Ivanovich, aspirant

Experimental study of the reaction of commutational and eddy currents in a transverse field amplidyne. Izv. vys. ucheb. zav.; elektromekh. 4 no.3:98-101 '61. (MIRA 14:7)

1. Zaveduyushchiy kafedroy elektrotekhniki Ul'yanovskogo politekhnicheskogo instituta (for Serdyuk). 2. Kafedra elektricheskikh mashin Tomskogo politekhnicheskogo instituta (for Skorospeshkin).  
(Rotating amplifiers)

SKOROSPECHNIK, Aleksey Ivanovich, kand. tekhn. nauk, doklad

Experimental study of the commutation of amplidynes. Izv. Vys.  
ucheb. zav.; elektromekh. 7 no.8:932-936 '64. (MIRA 17:10)

1. Kafedra elektricheskikh mashin Tomskogo politekhnicheskogo  
instituta.

SKOROSPESHKIN, Aleksey Ivanovich, kand.tekhn.nauk, dotsent; STEPANOV, Yuriy  
Andreyevich, inzh.

Amplisyn with a smooth rotor. Izv.vys.ucheb.zav.; elektromekh. 7  
no.10:1282-1283 '64. (MIRA 18:1)

1. Kafedra elektricheskikh mashin Tomskogo politekhnicheskogo  
instituta (for Skorospeshkin).



KOSTYL'OV, Boris Ivanovich, staryshiy prepodavatel'; SKOROSPESHKIN, Aleksey  
Ivanovich, kand. tekhn. nauk, dotsent; OBERGAN, Eduard Fomich, aspirant

Potential at the output of an amplidyne operating on a.c.  
Izv. vys. ucheb. zav.; elektromekh. 8 no. 9: 976-979 '65.

(MIRA 18:10)

1. Kafedra elektricheskikh mashin Tomskogo politekhnicheskogo  
instituta.

KRASIK, L.B.; YEGOROVA, A.I.; GEYKHMEN, K.P.; SKOROSPESHKINA, M.I.;  
KARKASHEVA, A.R.; PAREKHA, A.A.; GUZHAVINA, E.V.;  
STEPANOVA, N.I.

Physical development of pupils in the boarding schools of  
Perm (according to examination data of 1962). Zdrav. Ros.  
Feder. 7 no.6:22-26 Je '63. (MIRA 17:1)

1. Iz kafedry pediatrii (zav. - dotsent L.B. Krasik)  
Permskogo meditsinskogo instituta (rektor - dotsent T.V.  
Ivanovskaya).

MINCZEWSKI, Jerzy; SKORO-TRYBULA, Zofia

Reactions of 2-bromothiophene-3-hydroxamic acid with vanadium (V) and  
iron (III). Chem anal 5 no.1:163-165 '60. (EEAI 9:11)

1. Katedra Chemii Analitycznej Politechniki Warszawskiej  
(Vanadium) (Iron) (Hydroxamic acids)  
(Bromothiophene)

SKOROTSKIY, S.S.; LUKIN, S.V.; KORSHUNOV, I.V., red.; KHASIN, L.N., tekhn.  
red.

[Production planning for subsidiary plants of the petroleum trust]  
Proizvodstvennoe planirovanie podsobnykh predpriatii nefte doby-  
vayushchego tresta. Baku, Gos. nauchno-tekhn. izd-vo neft. i  
gorno-toplivnoi lit-ry, Azerbaidzhanskoe otd-nie, 1950. 124 p.  
(Petroleum industry) (MIRA 11:10)

DIL', A.; CHARUGINA, N.; BORODIN, A.; SOLODOVNIK, P.; SKLYAR, I.;  
SOLOVKIN, N.; POTAPOV, G.; PONOMAREV, N.; ALEKHIN, I. ;  
SOLOMENTSEV, K.; TOPYLIN, N.; SKOROVAROV, M.; KARABANOV, S.;  
BOGDANOV, N.; STRYUKOV, P.

Nikolai Vasil'evich Romenskii ( on the occasion of the 40th  
anniversary of his scientific, pedagogic, and public activity).  
Muk.-elev. prom. 24 no.12:29-30 D '58. (MIRA 12:1)  
(Romenskii, Nikolai Vasil'evich, 1894-)

Skorski K., Dr.

Skorski K., Dr. Ing. "Titanium and its Role in Steel Metallurgy." (Tytan i jego rola w metalurgii stali). Hutnik, No. 7-8, 1950, pp. 226-231, 5 figs., 2 tabs.

The common occurrence of titanium in nature, its chemical properties and compounds, are discussed. Titanium, as an alloy supplement to iron, increases several of the positive properties of steel. Enumeration of these properties. The author, taking for a basis the relatively cheap compound  $TiO_2$ , has produced  $Natim$ , for which he uses the term "titanek sodu". He produced this compound by melting  $TiO_2$  with  $NaCN$  in a graphite crucible. The product obtained after saking in  $1300^\circ C$ , lost sodium and passed probably into compound:  $Ti_{11}O_{24}N_4$ . This compound would be a very suitable deoxidising addition in the process of steel production.

SO: Polish Technical Abstracts - No. 2, 1951

~~SKOROV, B.M.~~ kandidat tekhnicheskikh nauk, redaktor; IZRAILOVICH, N.Ye.,  
Inzhener, redaktor; VORONIN, K.P., tekhnicheskii redaktor

[Progressive construction engineering] Peredovaya stroitel'naya  
tekhnika. Pod obshchei red. B.M.Skorova. Moskva, Gos.izd-vo  
lit-ry po stroit. i arkhitekt., 1952. 284 p. (MIRA 10:9)

1. Moscow. Tsentral'nyy institut informatsii po stroitel'stvu  
(Building)

SKOROV, B.M.

Housing construction abroad. Opyt stroi.no.4:4-12 '56. (MLRA 10:2)  
(Housing)



SKOROV, B.M., kandidat tekhnicheskikh nauk.

Lowering the weight of an apartment house is one of the means for  
reducing its construction cost. Biul. stroi. tekhn. 14 no. 4:9-12  
Ap '57. (MIRA 10:6)

1. Tsentral'nyy nauchno-issledovatel'skiy institut stroitel'stva Aka-  
demii stroitel'stva i arkhitektury SSSR.  
(Construction industry--Costs)

NOVIKOV, I.I., kand.iskusstv.nauk, arkhitektor; SKOROV, B.M., kand.  
tekhn.nauk, red.; MOROZOVA, G.V., red.izd-va; RUDAKOVA,  
N.I., tekhn.red.

[City building in foreign countries (France, the Netherlands,  
Belgium, Austria, and the German Federal Republic] Iz  
praktiki gradostroitel'stva za rubezhom (Frantsiia, Gollandiia,  
Bel'giia, Avstriia i FRG). Moskva, Gos.izd-vo lit-ry po stroit.,  
arkhit.i stroit.materialam, 1959. 73 p. (Opyt stroitel'stva,  
no.25) (MIRA 13:2)

(Europe, Western--City planning)

SKOROV, D.M.																									
PROCESSES AND PROPERTIES INDEX																									
<p>Heat treatment and choice of steels for complex cold punches. D. M. Skorov and S. I. Slutskii, <i>Kuchkovskaya Stal</i> 1936, No. 40, 55; <i>Chem. Zentr.</i> 1936, I, 4794-5.—Investigations are reported on the deformation of punches of complex form during hardening, together with the detn. of the most satisfactory heat treatment (from detns. of hardness and annealing temps.) for various types of steels alloyed with Cr, Ni, W and Mo.</p> <p>M. G. Moore</p>																									
<p>ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION</p>																									

SKOROV, D.M.

Choice of steels for dies and their heat treatment.

11. M. Skorov. *Kucheyennaya Stal* 1935, No. 10, 21-7. *Chem. Zvezda* 1936, 1, 419-7. Data are given on the chief types of breaks in dies and their causes, as well as the requirements for satisfactory dies. A review is included of die alloys preferred in America, England and Germany. Data are also reported on the heat treatment and use of 3 different die steels used in the Moscow Stalin Automobile Works. M. G. Moser

AS 4-51.4 METALLURGICAL LITERATURE CLASSIFICATION

<p>SKOROV D.M.</p> <p>CR</p>		<p>Choice of a steel and its best thermal treatment for the production of drift broaches. D. M. Skorov and A. I. Durokhov. <i>Vestnik Metalloprof.</i> 15, No. 4, 113-20 (1935); <i>Chem. Zentr.</i> 1936, I, 1002. Investigations are reported on alloyed steels of different C (0.2-1.7%), Cr and W contents with or without the addn. of Mo or V for the production of drift broaches which must show high resistance to shock and to wear together with a high degree of hardness and sufficient mech. strength. Steels of the following compns. are recommended: (1) 1.45-1.7% C, not less than 0.35% Mn, not less than 0.5% Si, 11-12.5% Cr, 0.15-0.3% V and 0.5-0.8% Mo; (2) 0.7-0.85% C, 1.25-1.75% Cr and 2.25-3.35% Mo; and (3) 0.2-0.1% C, 0.15-0.2% V and 0.15-0.2% Mo. The most satisfactory heat treatments were: (1) Heating to 790°, maintaining this temp. about 15 min. and cooling in a salt bath; (2) heating to 790°, maintaining that temp. 15 min., cooling 5 sec. in water and then cooling in oil; (3) heating as before to 790° and maintaining the temp. 15 min., cooling 10 sec. in water and then cooling in oil.</p> <p>M. G. Moore</p>	
<p>ANAL. SLA METALLURGICAL LITERATURE CLASSIFICATION</p>		<p>RECORD NUMBER</p>	

SKOROV, D.M.

6-12  
1-18

8696\* (Russian.) Some Properties of Zirconium-Niobium  
Alloys. Nekotorye svoystva splavov tsirkoniia s niobiem.  
In: E. Bychkov, A. N. Rozanov, and D. M. Skorov, *Atomnaya  
Energiya*, v. 2, Feb. 1957, p. 146-151.  
Preparation of alloys; constitution diagram; expansion at room  
temperature; heat resistance and hardness up to 750 C; aging  
properties.

3 'Sheet

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18

SKOROV, D. M.

27  
SOME PROPERTIES OF ZIRCONIUM-NIOBIUM ALLOYS.  
Yu. F. Bichkov, A. N. Rozanov, and D. M. Skorov. J. Nu-  
clear Energy B, 462-7(1957).

The constitution of zirconium-niobium alloys has been investigated and modifications to the existing equilibrium diagram are suggested. The mechanical properties of the alloys at room temperature have been determined and the hot-strength at temperatures of up to 750°C has been deduced from hardness measurements. Also, hardness has been measured after low-temperature ageing treatments. Measured results are correlated with the equilibrium diagram. The resistance of the alloys to oxidation in air has been determined in the temperature range 570 to 650°C.

(auth)

27/AE2C  
1-AE3d  
1-121

Skorov, D. M.

27  
"YOUNG'S MODULUS OF ZIRCONIUM-NIOBIUM ALLOYS.  
Yu. P. Bichkov, A. M. Rozhnov, and D. M. Skorov. J. Nu-  
clear Energy 3, 408-12(1957).

The results are given of measurements of the value of  
Young's modulus for zirconium-niobium alloys in vacuum  
at temperatures up to 550°C, and also at room temperature  
after various heat treatments (auth)

27 6-4E2C  
1-4E3d  
1-12



SOV/137-58-11-23615

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 11, p 249 (USSR)

AUTHORS: Bychkov, Yu. F., Rozanov, A. N., Skorov, D. M.

TITLE: Elastic Properties and Hardness of Zirconium-niobium Alloys at Elevated Temperatures (Uprugiyе svoystva i tverdos't' splavov tsi-rkoniya s niobiyem pri povyshennykh temperaturakh)

PERIODICAL: Sb. nauchn. tr. Mosk. in-t tsvetn. met. i zolota, Nauchnotekhn. o-vo tsvetn. metallurgii, 1957, Nr 30, pp 268-282

ABSTRACT: A Zr-Nb phase diagram is plotted. The mechanical and certain physical properties of alloys (A) thereof are investigated relative to temperature and time. The A are made in an arc furnace with a W electrode in an Ar atmosphere. The charge employed is Zr iodide containing 1.5% Hf also Nb foil with 1% Ta added. After repeated remelting, contamination with W is <0.1%. A with less than 20% Nb are forged at 800-500°C, while samples with greater Nb content are made from cast rods. The phase diagram plotted is identical in appearance with that of Rogers and Atkins (RZhMet, 1956, Nr 7, abstract 6709), but the transformation temperatures are somewhat lower owing to the difference in the chemical composition

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SOV/137-58-11-23615

## Elastic Properties and Hardness of Zirconium-niobium Alloys (cont.)

of the starting materials. The graph of  $H_B$  versus composition presents a flat maximum ( $260 \text{ kg/mm}^2$ ) at 50-80% Nb and a peak of diffusionless transformation at 7.5% Nb, which disappears upon slow cooling of the A from  $650^\circ$ . Quenched A are noticeably hardened by aging. As Nb content increases there is a rise in  $H_B$  at elevated temperatures, particularly at >20% Nb. Upon heating from  $20^\circ$  to  $750^\circ$  the hardness of A containing not less than 50% Nb is reduced by 20-30%, while when Nb content is about 7% the decline is by 95 to 97%. A study of the influence of A contents upon  $\rho$  makes it possible to clarify the dependence of E upon composition after various heat treatments. It is found that the strength of the interatomic bond in quenched Zr-Nb solid solutions is considerably less than the strength of the bond in pure Zr and in solid solutions with small additions of Nb. Distortion in the crystal lattice as the result of alloying and heat treatment results in a sharp change in E and  $\rho$ . Upon heating from 20 to  $900^\circ$  the value of E drops by 59% for Zr and only by 6.6% for A containing 75% Nb. At  $900^\circ$  all A have a substantially higher E than does pure Zr. Thus in Nb-rich A the properties characterizing heat resistance and the strength of the interatomic bond change considerably less than the properties of Zr-rich A in the same temperature intervals.

G. T.

Card 2/2

SKOROV, D.M.

PA - 2259

AUTHOR:

BYCHKOV, YU.F., ROZANOV, A.N., SKOROV, D.M.

TITLE:

Young's Modulus of the Alloys of Zirconium with Niobium  
(Modul' normal'noy uprugosti splavov tsirkoniya s niobiyem,  
Russian).

PERIODICAL:

Atomnaya Energiya, 1957, Vol 2, Nr 2, pp 152 - 156 (U.S.S.R.).  
Received: 3 / 1957

ABSTRACT:

The present work describes measuring results of this modulus in the vacuum at temperatures of up to 950° C and at room temperature after different forms of heat treatment.

At first the device for measuring this modulus is described by means of a drawing. Young's modulus was determined from the eigenfrequencies of bending flexural vibrations of cylindrical samples of a length of about 80 mm and a diameter of 4-6 mm. A normal telephone served as oscillation generator. The samples were produced in an electric arc furnace fitted out with a special device for casting rods in an argon atmosphere. The production of homogeneous viscous melts with a high content of niobium is discussed. For the purpose of investigating the influence exercised by heat treatment on Young's modulus, samples were annealed in evacuated quartz ampules in electric furnaces fitted out with heat regulators.

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The measured Young's modulus of tempered and annealed alloys as

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Young's Modulus of the Alloys of Zirconium with Niobium.

well as electric resistances of the tempered alloys are shown in form of diagrams. In the case of alloys tempered from  $1100^{\circ}\text{C}$  in water, the curves (Young's modulus to composition) and (electric resistance to composition) are mirrorimage-like assigned towards each other. The modification of the modulus and electric resistance are caused by distortions of the crystal lattice. The other factors exercise but little influence. The tempered alloys of niobium and zirconium are in a metastable state. Young's modulus of alloys shows a particularly marked increase in the vicinity of the minimum value of the modulus of the tempered samples. In a table it is shown in what manner Young's modulus of alloys with a different content of niobium decreases as a result of heating of these alloys from room temperature up to  $900^{\circ}\text{C}$ .

In conclusion the investigation of the transformations in zirconium-niobium alloys by means of the thermoelastic method is discussed in short. Thus, it is shown that an eutectoid transformation at  $560^{\circ}\text{C}$  in an alloy containing 10 % Nb occurs visibly in the case of heating. The creation of a new cubic  $\beta$ -phase in the case of heating the alloy above eutectoid temperature decreases Young's modulus rather sharply. Inverse transformation, decay of the  $\beta$ -phase into a hexagonal  $\alpha$ -phase and into a  $\delta$ -phase

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PA - 2259

Young's Modulus of the Alloys of Zirconium with Niobium.

of a different composition causes Young's modulus to increase.  
(3 illustrations and 1 table.)

ASSOCIATION: Not given.  
PRESENTED BY:  
SUBMITTED: 19.9.1956  
AVAILABLE: Library of Congress.

Card 3/3

32801  
S/137/61/000/012/121/149  
A006/A101

18.1272 1521 1418

AUTHORS: Bychkov, Yu.F., Rozanov, A.N., Skorov, D.M.

TITLE: Zirconium-niobium phase diagram

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no. 12, 1961, 23, abstract  
12Zh168 (V sb. "Metallurgiya i metalloved. chist. metallov", no. 1,  
Moscow, 1959, 179 - 191)

TEXT: The X-ray, thermal, dilatometric, thermal-elastic and metallographic methods were employed to study transformations and to plot a phase diagram of the Zr-Nb system. The alloys investigated were melted in an arc furnace in argon atmosphere from a Nb-strip of iodide Zr rods of 99.7% purity. After 3-5 fold remelting the ingots were forged at 800-600°C and subjected to heat treatment. It was established that in the Zr-Nb system at high temperatures a continuous series of solid solutions is formed between  $\beta$ -Zr and Nb with a minimum on the solidus curve at 1,600°C and 30% Nb. At 560°C, the eutectoid decomposition of  $\beta$ -solid solutions takes place. The eutectoid point corresponds to 12% Nb. During the quenching of alloys containing up to 15% Nb, the  $\beta$ -solution is

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32801

S/137/61/000/012/121/149  
A006/A101

Zirconium-niobium phase diagram

partially or fully transformed into acicular or reticular martensite-like structure. In alloys with 15% and more Nb, a body centered cubic  $\beta$ -phase appears during quenching from high temperatures. X

A. Belinkiy

[Abstracter's note: Complete translation]

Card 2/2

BYCHKOV, Yu.F.; KLIMOV, A.F.; ROZANOV, A.N.; SKOROV, D.M.

Effect of alloying on the longitudinal elasticity modulus of  
zirconium. Met.i metalloved.chist.met. no.1:231-242 '59.

(MIRA 12:10)

(Zirconium alloys) (Elasticity)



188300

S/137/61/000/005/056/060  
A006/A106

AUTHORS: Eyehkov, Yu. F.; Rozanov, A. N.; Skorov, D. M., and Cheburkov, V.I.

TITLE: Corrosion resistance of Li-T (Yai-T) steel in lithium with oxygen and nitrogen admixture

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no. 5, 1961, 60, abstract 5I453 (V sb.: "Metallurgiya i metallovedeniye chistykh metallov", no. 2, Moscow, Atomizdat, 1960, 78-92)

TEXT: The authors studied changes in the microstructure and mechanical properties of Fe, Ni, and Cr-Ni- steel grade "Yai-T" as a result of the effect of distilled Li and Li containing 1-2 weight % O or N. They investigated also changes in the chemical composition of Li due to the corrosion of the enumerated substances contained in it. /B

Ye. L.

[Abstracter's note: Complete translation]

Card 1/1

DASHKOVSKIY, A.I.; YEVSTYUKHIN, A.I.; SAVITSKIY, Ye.M.; SKOROV, D.M.

Temperature relation of internal friction and the shear modulus  
of uranium. Met. i metalloved. chist. met. no. 2:224-228 '60.  
(Uranium--Thermal properties) (MIRA 13:12)  
(Internal friction)

SAMONOV, A.M.; SKOROV, D.M.

Carbon distribution in ZHL, 1al-T and EL-211 stainless steels.  
Met. i metalloved. chist. met. no. 2;229-237 '60. (MIRA 13:12)  
(Steel, Stainless--Metallography)

SAMONOV, A.M.; SKOROV, D.M.

Studying the distribution of sulfur and phosphorus in ZHL,  
Ial-T and El-211 steels, by means of autoradiography. Met.  
i metalloved. chist. met. no. 2:238-251 '60. (MIRA 13:12)  
(Steel, Stainless--Metallography)

82282

S/089/60/009/01/05/011  
B014/B070

18.8200

AUTHORS: Dashkovskiy, A. I., Yevstyukhin, A. I., Savitskiy, Ye. M.,  
Skorov, D. M.

TITLE: Internal Friction of Uranium *A*

PERIODICAL: Atomnaya energiya, 1960, Vol. 9, No. 1, pp. 27 - 32

TEXT: The internal friction and, thus, the modulus of rigidity of uranium as dependent on temperature was measured by means of a relaxator which recorded the damping of the free torsional oscillations of a sample. A uranium wire of a length of 320 mm (diameter 0.98 mm) and a purity of 99.9% was used as a sample. The frequency of oscillations of the wire in a vacuum of  $5 \cdot 10^{-5}$  torr was  $\sim 2$ /sec. The rate of heating or cooling varied in the range  $5 - 0.5^{\circ}\text{C}/\text{min}$ . The accuracy of temperature measurement was  $\pm 1.5^{\circ}\text{C}$ . According to the three phases of uranium, the samples were annealed at 630, 645, 670, 720, 755, 768, 850, and  $960^{\circ}\text{C}$ . The course of the measured parameters is represented for the various temperatures in Figs. 1-5. The results of measurement lead to the

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Internal Friction of Uranium

82282

S/089/60/009/01/05/011  
B014/B070

following conclusions: (1) The bend in the internal friction curve in the temperature range 450 - 500°C is caused by the tenacity of the grain boundaries. This tenacity disappears after annealing in the  $\beta$ - and  $\gamma$ -phases. This is the result of the recrystallization of phases due to lower mobility of the boundaries. (2) In temperature changes, the polymorphous transformations of uranium are accompanied by an isothermal change in internal friction. The changes take place during heating as well as during cooling in both directions. (3) The most plastic  $\gamma$ -domain, which has a body-centered cubic lattice, is characterized by a high internal friction. The tetragonal  $\beta$ -modification which tends to brittleness, has the lowest internal friction. It is generally true that the internal friction is related directly to the crystal lattice and to its capability of plastic deformation. There are 5 figures and 13 references: 10 Soviet, 2 American, and 1 French. ✓

SUBMITTED: October 3, 1959

Card 2/2

PHASE I BOOK EXPLOITATION

SOV/5425

Fedorov, N.D., Candidate of Technical Sciences, Compiler

Kratkiy spravochnik inzhenera-fizika: Yadernaya fizika. Atomnaya fizika  
(Concise Handbook for the Engineering Physicist: Nuclear Physics. Atomic  
Physics) Moscow, Atomizdat, 1961. 507 p. 28,000 copies printed.

Ed.: A.F. Alyab'yev; Tech. Ed.: Ye. I. Mazel'.

PURPOSE: This reference book is intended for engineers and physicists working  
in the field of atomic and nuclear physics.

COVERAGE: The first seven parts of the book contain the most necessary reference  
material on atomic and nuclear physics. The remaining parts present information  
and data from other related fields. The last part gives the information on  
systems of units compiled from the new GOST specifications, physical constants,  
and some mathematical data. No personalities are mentioned. References  
accompany each part of the book.

Card 1/13.

Concise Handbook (Cont.)

SOV/5425

PART THREE. MATERIALS USED IN REACTOR CONSTRUCTION (D. M. SKOROV)

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I. Fuel elements	92
1. Metallic materials for fuel elements. 2. Ceramic fuel elements. 3. Dispersion type fuel elements. 4. Liquid fuel. 5. Basic materials used for the fabrication of fuel elements for the various types of reactors. 6. Materials for high-temperature fuel elements	
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1. Graphite 2. Beryllium 3. Ordinary water and heavy water. 4. Hydrides (solid)	
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Card-5/13	



CHEPKUNOV, V.V., aspirant[translator]; SKOROV, D.M., doktor tekhn. nauk, prof., red.; ZAVODCHIKOVA, A.I., red.; VLASOVA, N.A., tekhn. red.

[Metallography of reactor materials] Metallovedenie reaktor-nykh materialov; obzory. Moskva, Gosatomizdat. [From "Reactor Core Materials"; a quarterly...] Book 3. [Moderator, reflector, and control device materials] Materialy zamedlitel'ia, otrazhatelia i reguliruiushchikh ustroistv. Pod red. D.M.Skorova. 1962. 113 p. Translated from the ~~English~~ (MIRA 15:10)

1. Battelle Memorial Institute, Columbus, Ohio.  
(Nuclear reactors--Materials)

S/755/61/000/003/018/027

AUTHORS: Semenikhin, A.N., Gruzin, P.L., Skorov, D.M.

TITLE: The modulus of elasticity of beryllium at elevated temperatures.

SOURCE: Moscow. Inzhenerno-fizicheskiy institut. Metallurgiya i metallove-  
deniye chistyykh metallov. no.3. 1961, 190-192.

TEXT: The paper describes measurements of the dynamic modulus of normal elasticity (E) of Be at temperatures (T) up to 800°C. Be is an excellent nuclear moderator and neutron reflector; it has a small thermal-neutron-capture cross-section. Its major drawback is its brittleness, the reasons for which are as yet unknown. The E was calculated from the resonance frequency of flexural oscillation of a freely suspended cylindrical specimen. Measurements were made in a  $10^{-4}$ -torr vacuum on the equipment described by Bychkov, Yu.F., et al., in Atomnaya energiya, v.II, no.2, 1957. The specimens were 100 mm long, 5-mm diam, and were sintered of Be powder 99.8% pure. A mean E of 3 specimens at room T is 28,500 500 kg/mm<sup>2</sup>. The variation of E with T is linear up to 600°C, decreasing at a rate of 5.6 kg/mm<sup>2</sup> per °C. The steeper decrease in E in the 600-750° interval proceeds at 13.5 kg/mm<sup>2</sup> per °C. Comparison measurements on Zr, Ti, and X18H9T (Kh18N9T), steel indicate that the E of Be at 600° is about 3x that

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S/180/62/000/002/004/018  
E025/E535

AUTHORS:

Milov, I.V., Okinshevich, V.V. and Skorov, D.M.  
(Moscow)

TITLE:

On the temperature distribution in a rod in  
crucibleless zone recrystallization

PERIODICAL:

Akademiya nauk SSSR. Izvestiya. Otdeleniye  
tekhnicheskikh nauk. Metallurgiya i toplivo, no.2,  
1962, 56-62

TEXT:

The case is considered of the recrystallization of a  
cylindrical rod with the ends maintained at the fixed temperature  
 $T_2$  while the molten zone is maintained at the constant tempera-  
ture  $T_1$ . The molten zone is maintained by the supply of heat  
of power  $N$ . The liquid-solid boundary is assumed flat and  
perpendicular to the axis of the rod. It is assumed (1) that the  
loss of heat by evaporation in the solid phase is negligible,  
(2) the rod is in a vacuum and the heat exchange with the residual  
gases is negligible, (3) the heat flow from the walls of the  
chamber containing the rod onto the rod is negligible. A relation  
is obtained giving the distance from the molten zone as a  
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...tion depends on this. This can be

On the temperature distribution ... S/180/62/000/002/004/018  
E025/E535

done by programming the variation of cooling of the ends of the rod and, in the case of electron beam heating, by varying the emission current of the cathode as this is simpler than varying the voltage accelerating the electrons. In the case of induction heating the supply current of the inductor can be programmed. A study of the three dimensional problem of the temperature distribution in the rod is made by assuming the law of variation of the heat flow supplied to the rod along the length of the rod. Isothermal surfaces and lines of heat flow are sketched for this case. The condition is derived for the zone to be bounded by planes. The attempt to obtain a point focus for an electron beam in the case of electron ray heating is criticised on the ground that a point source leads to convexity of the zone boundaries and this convexity increases with the melting point of the material. It is stated that in induction heating the boundaries of the zone are concave. There are 5 figures. ✓

SUBMITTED: September 23, 1961

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SESSION NR: AT4005968

S/2755/63/000/004/0175/0181

AUTHOR: Milov, I. V.; Skorov, D. M.; Nikishanov, V. V.

TITLE: Mechanical properties of zone refined beryllium

SOURCE: Moscow. Inzhenerno-fizicheskiy institut. Metallurgiya i metallo-vedeniye chisty\*kh metallov, no. 4, 1963, 175-181

TOPIC TAGS: beryllium zone refining, beryllium property, beryllium micro-hardness, beryllium ductility, high purity beryllium, zone refined beryllium, beryllium zone melting, beryllium purification, beryllium mechanical property, beryllium

ABSTRACT: Wide application of beryllium as a structural material is limited because of its brittleness at room temperature. There are several techniques currently being tested for the production of plastic beryllium:

- (1) hot working of ingots, aimed at a certain orientation of crystallites;
- (2) alloying, aimed at fixation of the beta phase having a cubic lattice;

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Card

ACCESSION NR: AT4005968

- (3) grain refinement to 25 microns by powder-metallurgy processes;
- (4) purification by distillation, thermal decomposition of halides, and zone recrystallization.

Beryllium ingots were zone refined in a water-cooled copper crucible by the inert gas electric arc method, applying a zone propagation velocity of 0.75 mm/min. A columnar growth of grains was observed directly from the bottom and walls of the cooled crucible toward its axis and bending in the direction of the path of zone propagation. The length of the obtained grains reached 40-45 mm at a cross section of 2x3 mm. X-ray evidence did not disclose a clearly defined crystallographic orientation. Micro-hardness measurements, conducted at surfaces cut at right angles to the ingot axis, revealed that micro-hardness increases along the ingot in the direction of applied zone propagation. On the basis of micro-hardness measurements and crystallographic evidence, it was concluded that the basal plane, with small deviations, is oriented in the ingot at right angles to the direction of grain growth. This conclusion also confirmed the results of X-ray investigations.

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Specimens for compression tests, 7mm in diameter x 9mm long, were prepared from different regions of the zone refined ingots, choosing for the specimens a similar grain orientation. Beryllium plasticity is strongly dependent on preferred grain orientation and grain size. Basal planes (0001) in the test specimens were inclined approximately 50° with respect to their axes. Prepared specimens were compression tested on the recording type testing machine (TsNIITMASH-I) with a capacity of 4000 kg. The stress-strain curves obtained were similar to compression curves of plastic metals. The following mechanical properties were determined by compression testing of specimens taken from different locations along the ingot, and from ingots subjected to different numbers of zone refining passes: ultimate compressive strength, ultimate longitudinal strain, yield strength, longitudinal strain at yield stress. Specimens which have been cut from the zone-travel-starting-end, exhibited the greatest strength and ductility. The zone-travel-starting-end contained beryllium of higher purity, and the impurities migrated in the direction of zone propagation. It was concluded that strength and ductility of beryllium decreased with an increase of impurities content. It was observed that some of the failed test specimens were somewhat twisted around their axis. Difficulties arose in the investigations of deformation and plastic properties of polycrystalline beryllium when directions of grain growth during recrystallization were curvilinear in the

Card 3/4

MILOV, I.V.; OKINSHEVICH, V.V.; SKOROV, D.M.

Possibility for an extension of the pressure range measurement  
by the LT-2 thermocouple lamp. Zav. lab. 30 no.5:633 '64.  
(MIRA 17:5)

1. Moskovskiy inzhenerno-fizicheskiy institut.



SKOROV, G. Ye.

MANUKYAN, A.A.; GLUSHKOV, V.P.; SHVEDKOVA, V.M.; SVIRIDOVA, Z.P.; CHEBOTA-  
REVA, Ye.A.; SHUMILIN, V.I.; PUDINA, K.V.; BRAGINA, N.M.; LUTSKAYA,  
Ye.Ye.; KODACHENKO, A.S.; KOSOVA, V.A.; MOKLYARSKIY, B.I.; GRECHIKHIN,  
A.A.; KULIKOV, N.I.; RYDVANOV, N.F.; BEL'CHUK, A.I.; VINTSER, Yu.I.;  
ROZENTAL', Ye.I.; BELOUS, T.Ya.; SIDOROV, V.F.; ZHDANOVA, L.P.;  
ALEKSANDROVSKAYA, L.I.; KOVAL', V.V.; KHAVINSON, Ya.S., glavnyy red.;  
SOKOLOV, I.A., zam.glavnogo red.; ALEKSEYEV, A.M., red.; ARZUMANYAN,  
A.A., red.; BELYAKOV, A.S., red.; BECHIN, A.I., red.; VARGA, Ye.S.,  
red.; LEMIN, I.M., red.; LYUBIMOVA, V.V., red.; SKOROV, G.Ye., red.  
V redaktirovani uchashtvovali: SHAPIRO, A.I., red.; TATISHCHEV, S.I..  
KOVIRIGINA, Ye., tekhn.red.

[Economic conditions of capitalistic countries; review of business  
conditions for 1958 and the beginning of 1959] Ekonomicheskoe polo-  
zhenie kapitalisticheskikh stran; kon'iunkturnyi obzor za 1958 g.  
i nachalo 1959 g. Moskva, Izd-vo "Pravda," 1959. 127 p. (Prilo-  
zhenie k zhurnalu "Mirovaya ekonomika i mezhdunarodnye otnosheniia,"  
no.8, avgust 1959 g.) (MIRA 12:9)

1. Akademiya nauk SSSR. Institut mirovoy ekonomiki i mezhdunarodnykh  
otnosheniy. 2. Kollektiv sotrudnikov kon'yunkturnogo sektora Insti-  
tuta mirovoy ekonomiki i mezhdunarodnykh otnosheniy AN SSSR (for  
Glushkov, Shvedkova, Sviridova, Chebotareva, Shumilin, Pudina, Bragina,  
Lutskaya, Kodachenko, Kosova, Moklyarskiy, Grechikhin, Kulikov, Rydva-  
nov, Bel'chuk, Vintser, Rozental', Belous, Sidorov, Zhdanova, Alek-  
sandrovskaya, Koval'). (Economic conditions)

SHKROV, R. F.

SHKROV, R. F. "Control of Monilia on Apricots by Spraying with  
Creolin Solution," Sov. i Ogorod, no. 9, 1947, pp. 34-35. 80  
S413

SOURCE: SIRA 51-90-53, 15 Dec. 1953.

AUTHOR: Skorov, V.A.

136-58-3-2/21

TITLE: Molybdenum-Lead Products Selection Practice (Praktika selektsii molibdeno-svintsevykh produktov)

PERIODICAL: Tsvetnyye Metally, 1958, <sup>3</sup>/<sub>4</sub> Nr.3. pp. 7 - 10 (U.S.S.R.)

ABSTRACT: Consumer requirements fix the upper limit of lead in molybdenum concentrates at 0.3% and the author considers the selective flotation of a product of the following composition: 41.0 - 46.0% Mo, 3.2 - 9.7% Pb, 0.3 - 0.6% Cu, 0.02 - 0.07% Sn, 0.03 - 0.07% As, 0.02 - 0.05% P, 3.5 - 5.5% SiO<sub>2</sub>. A table showing the molybdenum and lead contents and distribution in the various size fractions and the size grading (table 1) indicates the need for further grinding. Laboratory work on the selective flotation of such materials started at the Chelyabinskii and continued at the Skopinskiy works, showed that grinding to 90% - 0.074 mm is needed. Flotation was effected in 3-% sodium sulphide solution with transformer oil as the collector, a recovery of molybdenum of over 98% being obtained in concentrate with a lead content of under 0.5%. The author next describes the full-scale scheme adopted (flowsheets figs.1 & 3) and the plant used (fig.2) (fig.2). The sodium-sulphide concentration was 2.5% and the resulting undesirably high concentration (1.6 - 1.7% Na<sub>2</sub>O + K<sub>2</sub>O) in the product necessitated washing. Temperature-control was found to be important, 40% being best for selective flotation of molybdenite and

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Molybdenum-Lead Products Selection Practice.

136-58-3-2/21

galenite. The concentrate contained less than 0.5% PG; a lead concentrate containing over 32% lead was also obtained, the loss of molybdenum in it being under 1% and the lead recovery being 90% of its content in the molybdenum-flotation tailings. The work showed the advantage of using solution from the thickening of molybdenum-flotation products. There are 3 figures and 2 tables.

ASSOCIATION: Skopinskaya obogatitel'naya fabrika (Skopinskaya Beneficiation Works)

AVAILABLE: Library of Congress.

1. Mining Industry-USSR
2. Ores-Production

Card 2/2

SKOROV, V.A.; GLUBOV, Yu.M.

Simultaneous retreatment of molybdenum concentration products  
of various composition. TSvet. met. 37 no.12:1-5 D '64  
(MIRA 18:2)

SKOROV, V.A.

Unified method of calculating marketable recovery in mineral dressing.  
TSvet, met. 34 no.2:19-24 F '61.. (MIRA 14:6)  
(Ore dressing)

SKOROV, V.A.

Dressing of tungsten substandard and collective rougher concentrates.  
TSvet. met. 34 no.3:4-10 Mr '61. (MIRA 14:3)  
(Ore dressing) (Tungsten ores)

SKOROV, V.A.; STEPANOV, I.S.; SHAKHNAZAROV, A.K., inzhener-metallurg,  
~~penzioner~~; PETROV, V.I., Geroi Sotsialisticheskogo Truda; BARYSHNIKOV,  
 I.F., starshiy inzhener; BUGAREV, L.A.; LAKERNIK, M.M., kand.tekhn.  
 nauk; SHEYN, Ya.P.; MOLCHANOV, A.A.

The greatest objective of our life. TSvet.met. 34 no.10:1-10  
 0 '61. (MIRA 14:10)

1. Glavnyy inzhener Skopinskogo zavoda "TSvetmet" (for Skorov).
  2. Zamestitel' predsedatelya Mezhdovedomstvennoy komissii po redkim metallam pri Gosudarstvennom komitete Soveta Ministrov SSSR po koordinatsii nauchno-issledovatel'skikh rabot (for Stepanov).
  3. Rukovoditel' brigady kommunisticheskogo truda elektroliznogo tsekha. Ural'skogo alyuminiyevogo zavoda (for Petrov).
  4. Otdel tsvetnoy metallurgii Gosplana SSSR (for Baryshnikov.).
  5. Nachal'nik podotdela otdela ekonomiki i razvitiya tsvetnoy metallurgii Gosekonomsoвета SSSR (for Bugarev).
  6. Zamestitel' direktora po nauchnoy chasti Gosudarstvennogo nauchno-issledovatel'skogo instituta tsvetnykh metallov (for Lakernik).
  7. Starshiy ekspert upravleniya Gosudarstvennogo komiteta Soveta Ministrov SSSR po avtomatizatsii i mashinostroyeniyu (for Sheyn).
  8. Glavnyy spetsialist otdela tsvetnoy metallurgii Gosplana SSSR (for Molchanov).
- (Communism)



SKOROV, Vasilii Andreyevich; TROITSKIY, A.V., otv. red.; GARBER, T.N.,  
red. izd-va; MAKSIMOVA, V.V., tekhn. red.

[Ore dresser] Obogatitel' gornorudnoi promyshlennosti. Moskva,  
Gosgortekhnizdat, 1961. 311 p. (MIRA 15:10)  
(Ore dressing)

SHAPIRO, K.Ya.; YURKEVICH, Yu.N.; SKOROV, V.A.

Treatment of intermediate molybdenum products for ammonium  
molybdate used in agriculture. TSvet. met. 35 no.9:67-70 S  
'62. (MIRA 16:1)

(Ammonium molybdate)

SKOROV, V.A.; GLEBOV, Yu.M.

Recovery of accessory minerals in finishing the dressing of  
intermediate products of tungsten. TSvet.met. 36 no.2:15-19  
F '63. (MIRA 16:2)

(Ore dressing--By-products)  
(Tungsten ores)

SKOROV, V.T.

Reply to the article "Required measure of labor productivity for  
signaling and communication workers." Avto., tele. i svyaz' 8  
no.8:36 Ag '64. (MLA 17:10)

1. Zamestitel' nachal'nika Barabinskoy distantsii signalizatsii i  
svyazi Zapadno-Sibirskoy dorogi.

L 18959-63

EPR/EWP(j)/EPF(c)/EWT(m)/BDS AFFTC/ASD Ps-4/Pc-4/Pr-4

RM/WW/MAY

ACCESSION NR: AP3006537

S/0191/63/000/009/0030/0033 81

AUTHORS: Trostyanskaya, Ye. B.; Kazanskiy, Yu. N.; Skorova, A. V.; Poymanov, A. M.; Snegireva, I. A.

TITLE: Determining the quality of glass cloth and glass roving sizing

SOURCE: Plasticheskiye massy\*, no. 9, 1963, 30-33

TOPIC TAGS: glass cloth sizing, glass, glass roving sizing, fiberglass water resistance

ABSTRACT: A method was worked out for evaluating <sup>15</sup>ACM-3 sizing and conditions were recommended for sizing <sup>15</sup>FN fiberglass with ACM-3. The amine number of the sizing film was determined by titration with HCl, readings being taken in the first couple minutes of the titration. The continuity of the sizing film was determined by electrically measuring the amount of moisture that would evaporate through the film, using an <sup>10</sup>IDN-142-meter, <sup>10</sup>ALM-2 voltmeter, and <sup>10</sup>KVTI/EN self-recording potentiometer. Orig. art. has: 7 figures, 1 equation.

Card

1/2

TROSTYANSKAYA, Ye.B.; POYMANOV, A.M.; SKOROVA, A.V.

Chemical reactions on the surface of glass fibers used for  
the production of glass reinforced plastics. Plast. massy  
no.11:67-69 '65. (MIRA 18:12)

L 20382-66 EWP(e)/EWT(m)/EWA(d)/EWP(j)/T/ETC(m)-6 WW/RM/WH

ACC NR: AP6006550 (A)

SOURCE CODE: UR/0191/65/000/011/0067/0069

AUTHORS: Trostyanskaya, Ye. B.; Poymanov, A. M.; Skorova, A. V.

92

B

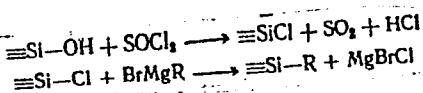
ORG: none

TITLE: Chemical reactions on the surface of glass fibers used in the manufacture of fiber-glass plastics,

SOURCE: Plasticheskiye massy, no. 11, 1965, 67-69

TOPIC TAGS: fiber glass, polymer, epoxy plastic, silicon quartz, surface active agent, glass fiber, silicon, glass, quartz, chemical reaction, surface ionization

ABSTRACT: It was the object of this investigation to find suitable conditions for the modification of surfaces of glass, silicon, and quartz fibers. The modification was carried out by the chemical addition of organic radicals to the surface, according to the schemes



and

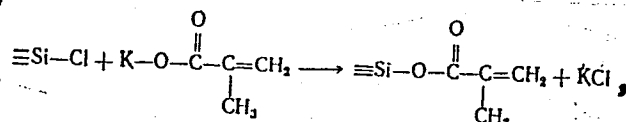
Card 1/2

UDC: 666.189.211:677.862.5

2

L 20382-66

ACC NR: AP6006550



where R = trimethylsilane, allyl, ethyl, phenyl, or methacryl respectively. The contact angle of wetting and electrical surface conductivity of the modified surfaces were determined after the method of Ye. B. Trostyanskaya, A. M. Poymanov, and Yu. N. Kazanskiy (Plast. massy, No. 7, 1964). The experimental results are tabulated. It was found that substitution of mono- and divalent ions by tri- and tetravalent ions on the modified surfaces enhances the hydrophobic nature of the latter and eliminates the retarding action of the surface hydroxyl groups on the rate of hardening of polycondensation type binders, thus improving the qualities of the fiber-glass plastics. Orig. art. has: 3 tables and 4 equations.

SUB CODE: 11/

SUBM DATE: none/

ORIG REF: 008/

OTH REF: 007

Card 2/2 vmb



24095

S/186/60/002/006/020/026  
A051/A129

26.2541

AUTHORS: Bagratsov, V. F.; Nikolayev, V. M.; Zolotarev, V. L.;  
Kostina, N.P.; Skrova, L. V.

TITLE: The sorption of microquantities of strontium and cesium on  
biotite

PERIODICAL: Radiokhimiya, v. 2, no. 6, 1960 734 - 738

TEXT: In a study of the sorption processes of strontium-90 and cesium-134 microquantities on biotite in the presence of macroquantities of alkali-earth metal and magnesium ions, the exchange equivalent and the applicability of the law of acting masses to the investigated system was established. The authors point out that the quantitative laws of ion exchange are expressed through the exchange isotherm. In deriving an equation for the ion exchange isotherm the activity coefficient of the microcomponent ion must be taken into consideration. The distribution coefficient concept (Ref. 12: S. Yu. Yelovich, ZhOKh, 3, 144, 660, 1953) is used. In case of sorption exchange of the microquantities of the element on the sorbent saturated by the macrocomponent, the ratio of the activity coefficients in the solid phase is a constant value, since the composition

Car 1/3

24095

S/186/60/002/006/020/026  
A051/A129

The sorption of microquantities of .....

of the solid solution changes very little, although the ionic strength of the solution can change here. Thus, the exchange constants are calculated for the investigated systems by determining  $B_0$  from experimental data. Biotite of the following composition was used in the experiments:  $SiO_2$ -35.74,  $Al_2O_3$ -13.92,  $Fe_2O_3$ -5.83,  $FaO$ -19.67,  $MnO$ -1.48,  $TiO_2$ -3.89,  $BaO$ -0.18,  $CaO$ -0.74,  $MgO$ -5.93,  $K_2O + Rb_2O + Cs_2O$  - 4.03,  $Na_2O$  - 3.38. The activity coefficient of the ions were

taken from literature data (Ref. 13: M. Kn. Karapet'yants, Khimicheskaya termodinamika. (Chemical thermodynamics). Goskhnimizdat, M.-L., 1953). The given isotherms of distribution show that the experimental results coincide favorably with the calculations, i. e., the interaction of cesium<sup>134</sup> and strontium<sup>90</sup> with biotite follows the law of acting masses. The value of  $G$  was found to be  $1.013 \cdot 10^{-5}$  mole  $Me^{2+}$  to 1 gram of sorbent. An anomalous bond strength was noted between the cesium ions and the sorbent. Finally, the following series of cation replacement on the biotite was derived from the calculated values of the exchange constants:  $Cs^+ > Ba^{2+} > Sr^{2+} > Ca^{2+} > Mg^{2+}$ . There are 2 tables, 2 figures and 16 references: 8 Soviet-bloc and 8 non-Soviet-bloc. The references to the four most recent English language publications read as follows: A. P. Vanselow, J. Am.

Card 2/3

24095

The description of microorganisms of ....

8/18/60/002/006/020/026  
A231/A.29

Chem. Soc., 54, 1927, 1928; A. F. Vassilow, Soil. Sci. 33, 95, 1932; J. Barchad,  
U. S. Min., 54, 1933, 1938; C. Barchad, U. S. Min., 34, 675, 1949.

SUBMITTED: January 18, 1949.

Card 3/C

PATOCKA, F.; MATA, M.; SOUCEK, A.; SOUCKOVA, A.; technical assistance:  
SKOROVA, Miroslava; SAMULOVA, Vera

Observations on the biological properties of atypical haemolytic  
Corynebacteria isolated from man as compared with Cor. haemolyticum,  
Cor pyogenes bovis and Cor. ovis. I. In vivo investigations.  
J. hyg. epidem. 6 no.1:1-12 '62.

1. Department for Medical Microbiology and Immunology, Charles  
University, Prague.  
(CORYNEBACTERIUM)

LASKORIN, B.N.; ZEFIROV, A.P.; SKOROVAROV, D.I.

[Extraction of uranium from solutions and pulp] Ekstraktsiia  
urana iz rastvorov i pul'p. Moskva, Glav. upr. po ispol'zo-  
vaniu atomnoi energii, 1960. 24 p. (MIRA 17:1)

S/089/60/008/06/04/021  
B006/B063 82305

21.3200

AUTHORS: Laskorin, B. N., Zefirov, A. P., Skorovarov, D. I.

TITLE: Extraction of Uranium From Solutions and Slimes

PERIODICAL: Atomnaya energiya, 1960, Vol. 8, No. 6, pp. 519-529

TEXT: The present paper gives data on the extraction of uranium from solutions and slimes of sulfuric, nitric, hydrochloric, and phosphoric acids by means of the esters of various acids, liquid cationites, and anionites. The authors discuss mainly methods which can be used in industry. They first describe the extraction of uranium from solutions. They studied the extraction with various organic compounds (e.g. alcohols, ethers, ketones, diketones, and their halogen derivatives, esters of various acids, aliphatic amides, etc.). Alcohols, ethers, and carboxylic acid esters extract uranium from nitric acid solutions. The selectivity of the acetic acid esters increases with their solubility in water, as may be seen from Table 1. The selectivity of the extracting agents decreases in the following order: carboxylic acid

X

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Extraction of Uranium From Solutions  
and SlimesS/089/60/008/06/04/021  
B006/B063 82305

esters, ethers, alcohols (Table 2). Fig. 1 shows the salting-out effect of  $\text{Ca}(\text{NO}_3)_2$  in the extraction of uranium by means of isoamyl acetate and dimethyl phthalate. Following this, the authors discuss the extraction by means of phosphoric acid esters. Trialkyl phosphates are well-known selective solvents for the extraction of uranium. The partition coefficient  $K_p$  which describes the extractibility, rises with an increase in the hydrocarbon radical up to  $\text{C}_5 - \text{C}_6$ , after which it drops exponentially. Triaryl phosphates practically do not extract uranium. The selectivity of trialkyl phosphates rises with increasing molecular weight of the extraction solvent. This may be seen from Table 3 which shows the dependence of  $K_p$  of uranium on the nature of the hydrocarbon radicals of the phosphoric acid esters. The technological process of the extraction of uranium from nitric acid desorption solutions is schematically represented in Fig. 3. The authors next discuss the extraction of uranium by means of diisoamyl esters of methyl phosphinic acid  $[\text{i}(\text{C}_5\text{H}_{11}\text{O})_2\text{POCH}_3]$  (DAMFK). Figs. 4 and 5 show the dependence of  $K_p$  on the content of hydrochloric acid and phosphoric acid of the solution from which uranium is extracted. Analogously, the

Card 2/3

X

Extraction of Uranium From Solutions  
and Slimes

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authors discuss the extractibility of trioctyl phosphin oxide ( $C_8H_{17})_3PO$ , dialkyl phosphites  $[(RO)_2P(OH)]$  with hydrocarbon radicals from  $C_4$  to  $C_8$ , alkyl phosphoric acids, and amines. Alkylamines and alkyl-arylamines with long chains extract uranium from sulfuric acid solutions and concentrated hydrochloric and nitric acid solutions similarly as ion-exchange resins. The  $K_p$  values for U VI are given in Table 4 for numerous amines. Fig. 8 gives the technological scheme for a special case. The last part of the present paper treats the extraction of uranium from ore slimes. The losses of the extraction solvent are discussed, and it is shown that these losses decrease with increasing content of solid substances in the ore slimes or pastes (Fig. 9). The extraction of uranium from an ore paste is schematically shown in Fig. 10 and described. There are 10 figures, 4 tables, and 7 references: 6 Soviet and 1 Yugoslavian.

SUBMITTED: July 18, 1959

Card 3/3

X



S/830/62/000/001/008/012  
E079/E192

AUTHORS: Laskorin, B.N., Skorovarov, D.I., and Shatalov, V.V.

TITLE: Extraction of uranium with trioctylphosphin oxide

SOURCE: Ekstraktsiya; teoriya, primeneniye, apparatura.  
Ed. by A.P. Zefirov and M.M. Senyavin.  
Moscow, Gosatomizdat, 1962. 163-170

TEXT: The main extracting properties of trialkylphosphin oxides are illustrated on trioctylphosphin oxide (TOPO). Taking into consideration that the saturation of TOPO is attained already at an equilibrium concentration of uranium in aqueous phase (about 1 g/l) and that at low initial concentration of uranium TOPO retains a high capacity, coefficients of distribution of uranium on extraction with 0.1 M solution of TOPO in kerosene from nitrate solutions with a low uranium content (965-0.08 mg/l) were determined. With decreasing concentration of uranium in the aqueous solution, the coefficient of distribution increases and reaches 20,000. The influence of the concentration of nitric and hydrochloric acids on the extraction of uranium was also determined. The salting out action of nitric acid is evident to a concentration

Card 1/2

LASKORIN, B.N.; SKOROVAROV, D.I.; SHATALOV, V.V.

Extraction of uranyl nitrate from nitric acid desorption solutions  
by tributyl phosphate and other organosphorous compounds. El-str.;  
teor.,prim.,app. no.2:174-178 '62. (MIRA 15:9)  
(Uranyl nitrate) (Phosphorous organic compounds)

LASKORIN, B.N.; GOLYNKO, Z.Sh.; SKOROVAROV, D.I.

Extraction of uranyl sulfate by tri-n-octylamine. Ekstr.; teor.,  
prim., app. no. 2:190-198 '62. (MIRA 15:9)  
(Uranyl sulfate) (Octylamine)

LASKORIN, B.N.; SKOROVAROV, D.I.; FILIPPOV, Ye.A.; SHILIN, A.L.

Mixtures of mono- and di(2,4-diethyl-1-octyl) methyl phosphonates  
as extractants. Radiokhimiia 5 no.4:424-428 '63. (MIRA 16:10)

(Phosphonic acid)

(Extraction (Chemistry))

E 63622-65 EPF(n)-2/EPF(m)/EPF(b)/EPF(t) Pu-4 IJP(c) WW/JD/JG 22  
 UR/0186/65/007/003/0356/0357 21  
 542.61:546.791.6:661.718.1+661.718.2 B  
 ACCESSION NR: AP5017002

AUTHOR: Laskorin, B. N.; Filippov, Ye. A.; Goncharenko, G.I.; Skvortsov, N. V.;  
Skorovarov, D.I.

TITLE: Extraction of uranium (VI) from carbonate solutions by quaternary phosphonium and  
 arsonium bases

SOURCE: Radiokhimiya, v. 7, no. 3, 1965, 356-357

TOPIC TAGS: uranium extraction, phosphonium base, arsonium base, hydroxyquinoline

ABSTRACT: To determine the effect of the concentration of carbonate ions and nature of  
 the diluent on the extraction of uranium (VI), the authors tested phosphonium salts  
 $[R_4P]^+Cl^-$  and arsonium salts  $[R_4As]^+Cl^-$ . The organic phase consisted of a 0.1 M  
 solution of the quaternary base in chloroform or butyl ethyl ketone containing 7 vol. %  
 n-octanol. 0.008 M aqueous solutions of uranium containing 0.1 M ammonium bicarbon-  
 ate and 0.1-1.0M sodium carbonate were employed. The extraction was carried out by  
 vigorously shaking the combined aqueous and organic phases. It was found that the arsonium  
 and phosphonium compounds have practically the same extractive properties, but the addi-  
 tion of 8-hydroxyquinoline causes the distribution ratio to be much higher in the case of the  
 arsonium compounds. It is concluded that the extraction of uranium (VI) from carbonate

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L 63622-65

ACCESSION NR: AP5017002

media by the phosphonium and arsonium compounds is rather ineffective owing to a decrease in the distribution coefficient caused by an appreciable solubility of the complex in the aqueous phase; however, the addition of 8-hydroxyquinoline raises the distribution ratio because of the formation of the complex  $[\text{UO}_2(\text{C}_9\text{H}_6\text{ON})_3]^-$ , which has no affinity for water. "The phosphonium and arsonium bases were synthesized by G. Kh. Kamay and co-workers." Orig. art. has: 3 figures and 4 formulas.

ASSOCIATION: None

SUBMITTED: 23Dec63

NO REF SOV: 000

ENCL: 00

SUB CODE: IC

OTHER: 007

Card

2/2

12

0.7

Effect of temperature and sulfur dioxide gas on *Bruchus pisi*, a parasite of peas. M. Skurvyayev. *Makomol's* 12, No. 6, 47-8(1937); *Chimie & industrie* 40, 997.—Peas cannot be completely rid of *Bruchus pisi* either by drying or by treatment with SO<sub>2</sub>. The degree of contamination of the peas can be lowered, however, by drying; and when they are dry they can be heated to 50° by means of a heat vehicle at a temp. of 110-20°, without splitting; when heated with steam, on the other hand, the peas split in half. A. Papineau-Couture

ASS-SLA METALLURGICAL LITERATURE CLASSIFICATION

SKOROVAROV, M., inzhener

For early drying of moist grain delivered for seed and for food.  
Muk.-elev.prom.21 no.9:4-5 S'55. (MIRA 8:12)

1. Ministerstvo zagotovok  
(Grain--Drying)



SKOROVAROV, M., inzhener; ZHOGOLEV, Ye., inzhener.

Experimental mobile grain dryer installed in a railroad car.  
Muk.-elev.prom. 21 no.12:13-15 D '55. (MLRA 9:4)  
(Grain--Drying)

SKOROVAROV, Mikhail Antonovich; KEYZER, V.A., redaktor; GOLUBKOVA,  
L.A., tekhnicheskiiy redaktor

[The operation of grain dryers; a manual for grain drying foreman]  
Ekspluatatsiia zernosushilok; posobie dlia masterov zernosusheniia.  
Moskva, Izd-vo tekhn. i ekon. lit-ry po voprosam mukomol'no-  
krupianoj, kombikormovoi promyshl. i elevatorno-skladskogo  
khoziaistva-Khleboizdat, 1956. 165 p. (MLRA 10:4)  
(Grain--Drying)

SKOROVAROV, M.A., inzhener.

What hinders inventing in the Ministry of the Bread-Baking Industry?  
Izobr. v SSSR 1 no.6:37-38 D '56. (MLA 10:4)  
(Inventions) (Baking)

SKOROVAROV, M., inzhener.

~~XXXXXXXXXXXXXXXXXXXX~~  
Making efficient use of grain drying equipment. Muk.-elev. prom.  
22 no.8:3-5 Ag '56. (MIRA 10:8)

1. Tekhnicheskiiy otdel Ministerstva khleboproduktov SSSR.  
(Grain drying)